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LOW DENSITY INORGANIC FOAMS FABRICATED USING MICROMAVES

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ABSTRACT

The objective of our work was to determine if high temperature foams could be made using microwave heating; and if so, to investigate some of their properties. Several foams were made and their compressive strengths, tensile strengths and densities were determined. Foams were made of glass, metal-glass, glass-fiber, metal-glass-fiber, and fly ash. The microwave source used was a Litton model 1521 microwave oven which operated at 2.45 GHz and had an output of 700 watts.

Introduction

The history of microwave heating of oxide materials dates back at least to the work of Von Hippel in the late 1940's. His interest was in how the loss characteristics of these materials varied as a function of frequency. Over the last 25 years little has been published in this area; however, work has been done at GMC, and at the University of Edmonton in Edmonton, Alberta Canada by W. Tinga.

This paper addresses some preliminary work done at Los Alamos on the fabrication of low density structures using microwave heating. Several glass, glass-ceramic, and glass-metal-ceramic systems were investigated and will be discussed in this paper. Some mechanical properties will be reported on along with microstructural information.

Preparation of Foams

Table I lists the different foams prepared and Table II shows the composition of some foams. It was decided to fabricate foams initially from glass microballoons and metal microballoons using a glass binder (in this case potassium silicate) which also acted as a microwave coupling agent and foaming agent. The glass microballoons were obtained from 3M Company and were a typical soda lime silicate glass with size distribution of from 3N microns to 130 microns. The metal microballoons were obtained from International Harvester Company and were composed of mainly nickel with some silicon and manganese. Their size ranged from around 400 microns to 600 microns. Also used to make foams was fly ash microballoons, a by produce of coal fired electrical generating facilities. Table VII shows the exact composition of the microballoons used. Several foams initially were made by mixing various microballoons with potassium silicate and then heating in a microwave oven. Densities of these foams are listed in Table VI, the F series foams are the first generation foams and the T series foams are the second generation foams that have been fabricated using microwave heating.

From Table II it is seen that many materials were used as microwave coupling agents. A coupling agent is a material that at room temperature will absorb microwave energy at 2.45 GHz (usually materials with OH, CO, NO, or NH bonds). This material will heat at 2.45 GHz and raise the surrounding temperature of the ceramic or glass thus increasing their loss tangent and increasing their microwave coupling efficiency. Along with the requirement that the coupling agent couple well to 2.45 GHz microwave radiation, the coupling agent also had to form a strong bond with the foam material in order to improve the foam mechanical properties.

Typical fabrication procedure was to mix by weight microballoons as shown in Table I with a suitable coupling agent as shown in Table III. The mixture was then placed into a reaction cavity inside a model 1521 Litton microwave oven (shown in Fig. I) and heated for between five minutes and 30 minutes in air.

Foam Microstructures

Figures II-IV show SEM photomicrographs of several of the foams discussed above. In all cases the coupling agent glass used formed excellent bonds with the microballoons used. Of interest is the wetting of the glass binder material and the metal microballoons. Excellent adherence is seen between the glass binder and the metal microballoons yet relatively low temperatures were measured (less than 600°C for ten minutes). Also of interest were the foams in which were used SiC fibers. Mechanical strength data indicates no beneficial effect of the SiC fibers on foam integrity. This is probably because processing temperatures were not high enough to form strong bonds between the microballoons, glass binder and the SiC fibers. Also fiber geometry was not optimized to improve packing density. Table 3 lists the coupling agent binder glasses used. The higher temperature binder glasses generally resulted in improved mechanical properties.

Mechanical Properties

The sample configurations shown in Fig. V and Fig. VI were used to obtain compressive strength and tensile strength data on the foams listed in Table I.

As seen in Table IV the strongest foams in tension were T-5, T-8, and T-13 and in compression were T-12, T-11, T-10, and T-7 as shown in Table V. All of these foams had as a major phase fly ash except for 1-5 and T-7 which were composed of glass and metal microballoons and either a low temperature glass binder with potassium silicate or just potassium silicate used as a coupling agent and a binder itself. A variable that differed from samples T-5 and T-7 and the fly ash samples was exposure time to the microwave radiation. The fly ash foams were heated for fifteen minutes while the non fly ash foams were heated only six minutes. Probably higher temperatures were reached in the fly ash foams; however, this is not known for certain because no good method has been found for measuring temperature in a microwave environment. If appreciably higher temperatures were achieved in the fly ash foam then phases could have been formed which resulted in superior mechanical properties.

The lowest density foams were made using either fly ash 40.09 g/cm^3) or metal microballoons with potassium silicate, also 0.09 g/cm^3 .

Conclusions

The work described in this paper is preliminary in nature and much further work needs to be done to better relate observed mechanical properties to processing parameters. Much more detailed microstructural analysis needs to be done to correlate structure with foam composition, and foam mechanical properties. It has been demonstrated, however that inorganic low density foams can be fabricated using microwave energy, and mechanical properties obtained to date indicate that these foams can be machined and used perhaps for structural components in space.

Further work to improve foam tensile and compressive strength is in progress. By varying the microwave processing time and foam binder composition and using proper geometry fibers, better foam mechanical properties may result.

Acknowledgements

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- Figure I Microwave reaction cavity used to prepare the foams.
- Figure II Shown is a 200X view of a broken glass bond between two metal microballoons (Trade name Solacel).
- Figure III Shown is a 2000X view of glass bonds between glass micro-balloons.
- Figure IV Shown is a 2000X view of glass bonds between glass microballoons and a metal microballoon.
- Figure V Shown is a machined foam sample ready for obtaining tensile strength data.
- Figure VI Shown is a machined foam sample ready for obtaining compressive strength data.

TABLE I FOAMS FABRICATED USING MICROWAVE HEATING

FLY ASH + C

GMB + C

GMB + SiC FIBERS + C

GMB + MB + C

GMB + MB + FIBERS + C

MB + C

MB + FIBERS + C

GMB = glass microballoons
MB = metal microballoons
C = coupling agent

TABLE II

COMPOSITION OF SELECTED FOAMS

- F-1 Potassium Silicate 22.8 g 3M Glass Bubbles - 9.7 g
- F-2 Potassium Silicate 22.8 g 3M Glass Bubbles - 8.5 g SiC Fibers - 0.9 g
- F-3 Potassium Silicate 22.8 g
 3M Glass Bubbles 7.3 g
 SiC Fibers 0.9 g
 Metal Beads 0.5 g
- F-4 Potassium Silicate 27.8 g 3M Glass Bubbles - 7.3 g Metal Beads - 0.5g
- F-5 Potassium Silicate 22.8 g 3M Glass Beads - 4.9 g Metal Beads - 3.1 g
- F-6 Potassium Silicate (enough potassium silicate was used to bind the metal microballoons together) Fly Ash 57.0 g Hydrated KSiO₄ 61.2 g

TABLE III COUPLING AGENTS USED

GLYCEROL

NITRATES

POTASSIUM SILICATE

SODIUM SILICATE

1613 GLASS

OI 0338 GLASS

OI 1756C GLASS

TABLE IV
TENSILE STRENGTH OF FOAMS

SAMPLE	TENSILE STRENG	TH (psi)
T-1-1	1.03	(149)
-2	1.24	(180)
-3	1.01	(146)
T-2-1	1.17	(170)
-2	1.21	(176)
-3	1.10	(159)
T-3-1	0.93	(135)
-2	0.78	(113)
-3	0.70	(101)
T-4-1	0.99	(144)
-2	0.68	(98)
-3	0.24	(34.5)
T-5-1	1.21	(176)
-2	2.76	(400)
-3	3.24	(470)
T-6-1	0.74	(108)
-2	1.13	(164)
T-7-1	1.56	(226)
T-8-1	2.34	(340)
-2	1.76	(255)
-3	0.62	(90)
T-9-1	0.93	(135)
-2	0.39	(56)
-3	0.81	(118)
T-10-1	0.54	(54)
-2	0.81	(118)
-3	1.01	(146)
T-11-2	1.35	(196)
T-12-1	1.09	(158)
T-13-1	0.66	(96)
-2	1.05	(153)
-3	2.41	(350)
T-14-1	1.35	(196)
-2	0.34	(50)
-3	1.35	(196)
T-15-1	0.74	(107)
-2	0.50	(73)

TABLE V

COMPRESSIVE STRENGTH OF FOAMS

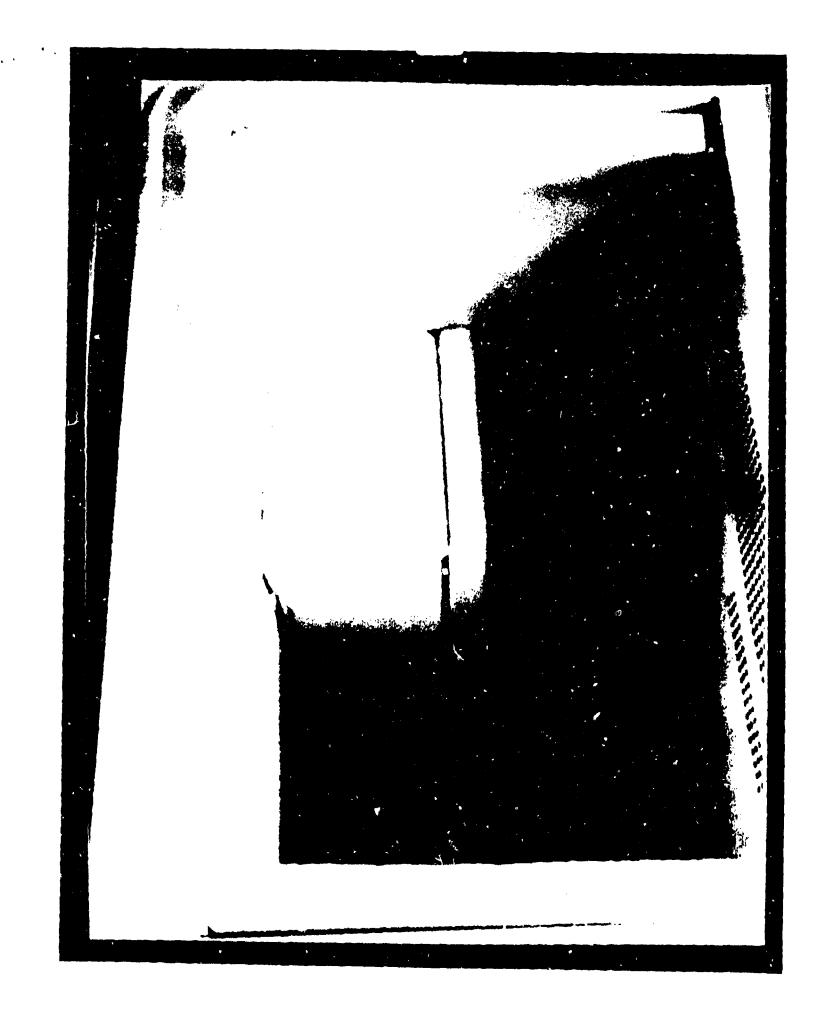
SAMPLE	COMPRESSIVE	STRENGTH
	MPA	(psi)
T-4-4	2.79	(405)
-5	3.17	(460)
T-5-4	3.79	(550)
-5	3.79	(550)
T-6-4	3.17	(460)
-5	2.96	(430)
T-7-2	3.96	(575)
-3	4.38	(635)
T-8-4	3.10	(450)
T-9-4	2.41	(350)
-5	2.96	(430)
-6	3.07	(445)
T-10-1	4.76	(690)
T-11-3	4.89	(710)
-4	2.52	(365)
T-12-2	4.07	(590)
-3	5.38	(780)
T-13-4	3.34	(485)
-5	3.41	(495)
-6	2.90	(420)
T-14-4	2.86	(415)
-5	2.55	(37(
-6	2.86	(415)
T-15-3	3.79	(550)
-4	3.86	(560)

TABLE VI FOAM DENSITIES

SAMPLE #	DENSITY g/cc
F1	0.14
F2	0.32
F3	0.30
F4	0.28
F5	0.24
T1	0.30
Т2	0.34
Т3	0.33
T4	0.19
T5	0.27
Т6	0.09
T7	0.32
Т8	0.11
Т9	0.09
T10	0.13
T11	0.14
T12	0.12
T13	0.16
T14	0.41
T15	0.40

TABLE VII
Microballoon Composition

Microballoon	Material	Weight %
	No. O	5.6
Glass	Na ₂ 0	
	\$10 ₂	85.3
	CaO	9.1
Solacel	Ni	74
	Mn	24
	Si	2
Fly ash	S10 ₂	57.1
	^{A1} 2 ⁰ 3	31.2
	K ₂ 0	5.4
	Fe0	5.2
	T10 ₂	1.1





200X



2,000X



2,000X



